

**VMS 2008**

Workshop on Variational Multiscale Methods

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# An Algebraic Variational Multiscale-Multigrid Method for Large Eddy Simulation of Turbulent Flow



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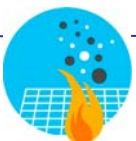
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Technical University of Munich



# Outline

- Three-Scale Variational Multiscale LES
  - Algebraic Multigrid Scale Separation
    - Fourier Analysis
- Numerical Examples



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# Three Different Approaches to LES

## **Traditional LES (introduced 1960s, e.g., books by Geurts, John, Sagaut)**

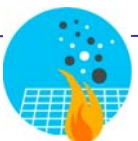
- resolved + unresolved scales, scale separation via (implicit) filtering
- various models, one widely-used option: (dynamic) subgrid-viscosity model

## **Three-Scale VMLES (introduced Hughes et al. (2000) + various authors)**

- coarse + fine resolved + unres. scales, scale separation via variat. projection
- dominating model option so far: (dynamic) subgrid-viscosity model

## **Residual-Based VMLES (introduced Calo (2004) + e.g., Bazilevs (2007))**

- resolved + unresolved scales, scale separation via variational projection
- modeling: approximate analytical representation -> stabilized methods





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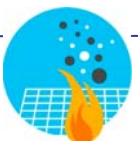
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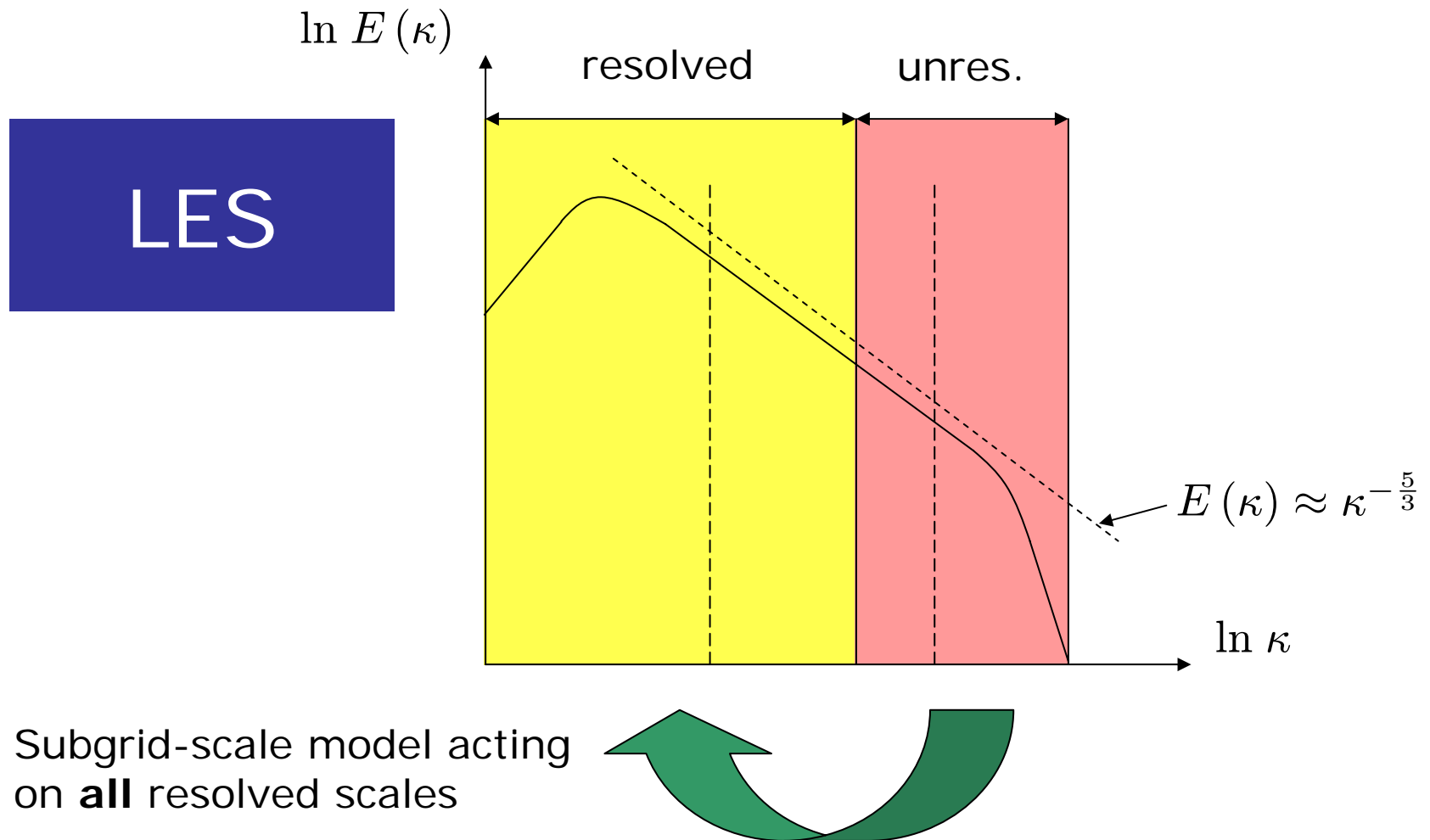
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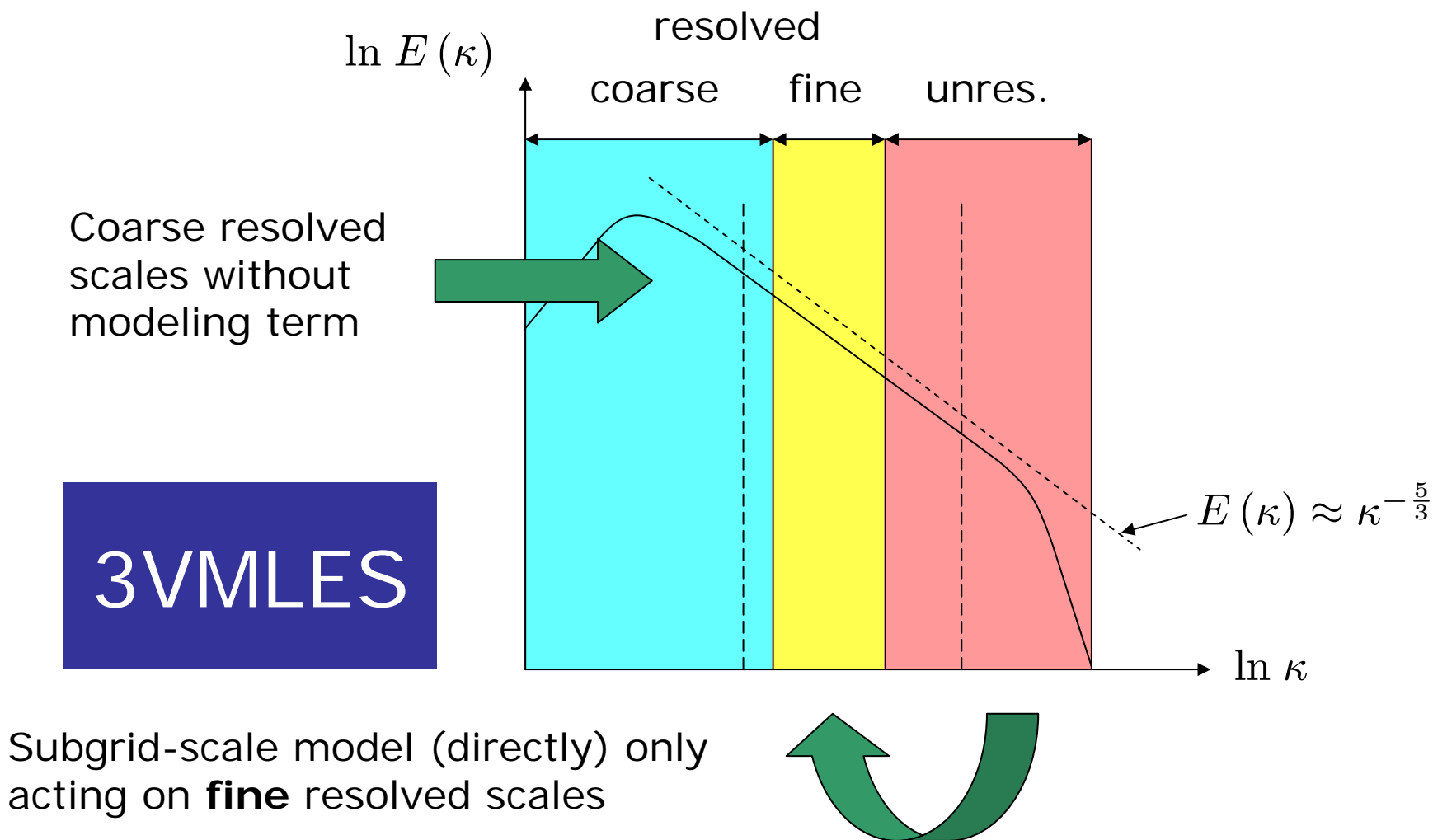
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# Kolmogorov Energy Spectrum: Traditional LES

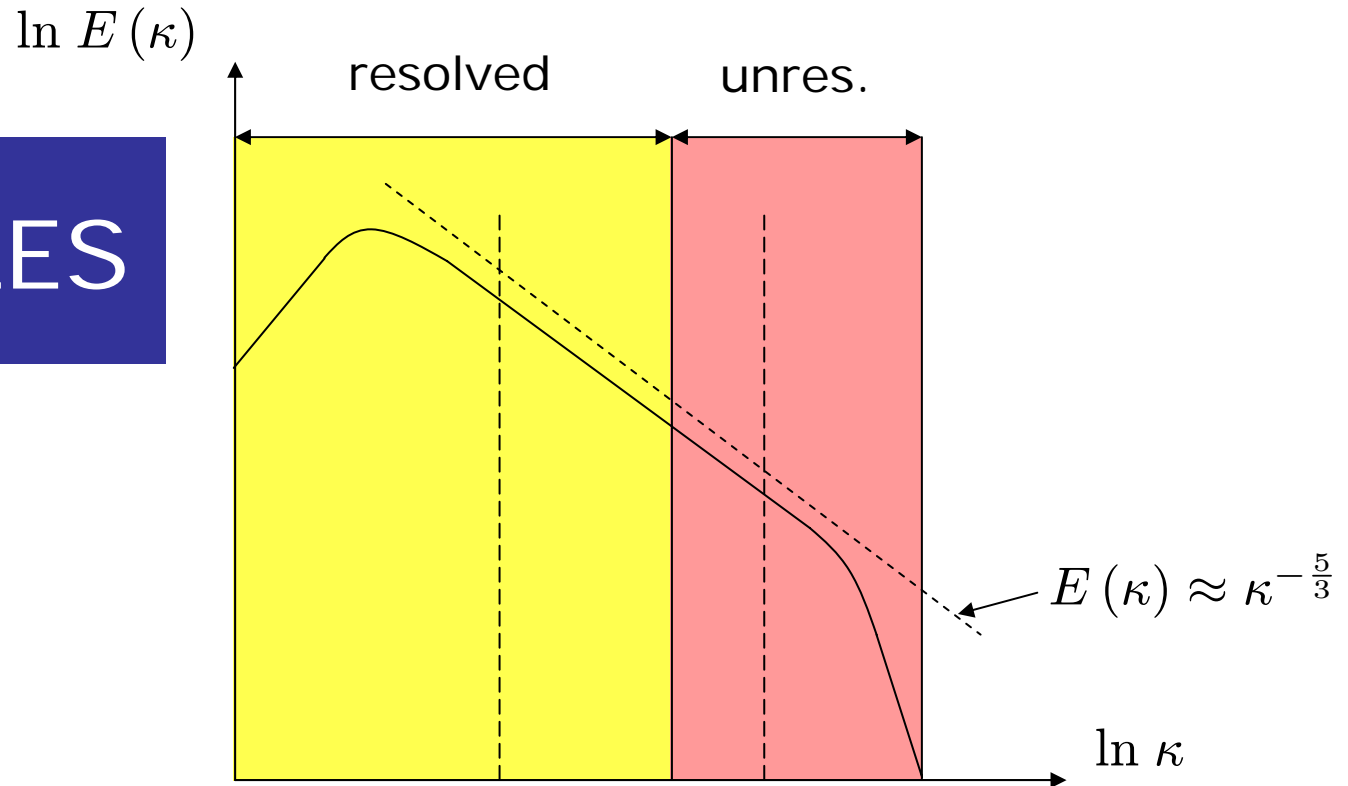


# Kol. Energy Spectrum: Three-Scale VMLES

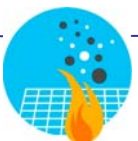
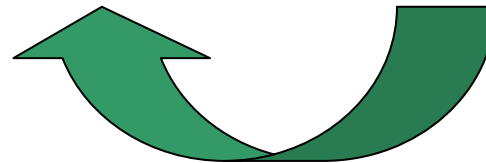


# Kol. Energy Spectrum: Residual-Based VMLES

RBVMLES



**Unresolv.-scale approxim.**  
acting on **all** resolved scales



# Strong and Weak Formulation of Navier-Stokes

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{u} \otimes \mathbf{u}) - 2\nu \nabla \cdot \varepsilon(\mathbf{u}) + \nabla p = \mathbf{f} \quad \text{in } \Omega \times ]0, T] \quad (\text{momentum equ.})$$

$$\nabla \cdot \mathbf{u} = 0 \quad \text{in } \Omega \times ]0, T] \quad (\text{continuity equ.})$$

$$\mathbf{u} = \mathbf{g} \quad \text{on } \Gamma_g \times ]0, T] \quad (\text{Dirichlet b.c.})$$

$$\sigma \cdot \mathbf{n} = \mathbf{h} \quad \text{on } \Gamma_h \times ]0, T] \quad (\text{Neumann b.c.})$$

$$\mathbf{u} = \mathbf{u}_0 \quad \text{in } \Omega \times \{0\} \quad (\text{initial condition})$$

$$B_{\text{NS}}(\mathbf{v}, q; \mathbf{u}, p) = B_{\text{M}}(\mathbf{v}; \mathbf{u}, p) + B_{\text{C}}(q; \mathbf{u}) = (\mathbf{v}, \mathbf{f})_{\Omega} \quad \text{where}$$

$$B_{\text{M}}(\mathbf{v}; \mathbf{u}, p) = \left( \mathbf{v}, \frac{\partial \mathbf{u}}{\partial t} \right)_{\Omega} + (\mathbf{v}, \nabla \cdot (\mathbf{u} \otimes \mathbf{u}))_{\Omega} + (\varepsilon(\mathbf{v}), 2\nu \varepsilon(\mathbf{u}))_{\Omega} - (\nabla \cdot \mathbf{v}, p)_{\Omega}$$

$$B_{\text{C}}(q; \mathbf{u}) = (q, \nabla \cdot \mathbf{u})_{\Omega}$$



# 3-Scale Velocity Separation

[Hughes et al. (2000), Collis (2001), Gravemeier (2003), ...]

3-scale separation of velocity weighting/solution functions + funct. spaces:

$\mathcal{V} = \overline{\mathcal{V}}^h \oplus \mathcal{V}'^h \oplus \hat{\mathcal{V}}$	$\mathcal{S} = \overline{\mathcal{S}}^h \oplus \mathcal{S}'^h \oplus \hat{\mathcal{S}}$	$\mathbf{v} = \overline{\mathbf{v}}^h + \mathbf{v}'^h + \hat{\mathbf{v}}$	$\mathbf{u} = \overline{\mathbf{u}}^h + \mathbf{u}'^h + \hat{\mathbf{u}}$
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3 subproblems:      coarse resolved + fine resolved + unresolved scales

$$B_M(\overline{\mathbf{v}}^h; \overline{\mathbf{u}}^h + \mathbf{u}'^h + \hat{\mathbf{u}}, p^h + \hat{p}) = (\overline{\mathbf{v}}^h, \mathbf{f})_\Omega \quad \longrightarrow \text{coarse-scale eq.}$$

$$B_M(\mathbf{v}'^h; \overline{\mathbf{u}}^h + \mathbf{u}'^h + \hat{\mathbf{u}}, p^h + \hat{p}) = (\mathbf{v}'^h, \mathbf{f})_\Omega \quad \longrightarrow \text{fine-scale eq.}$$

$$B_M(\hat{\mathbf{v}}; \overline{\mathbf{u}}^h + \mathbf{u}'^h + \hat{\mathbf{u}}, p^h + \hat{p}) = (\hat{\mathbf{v}}, \mathbf{f})_\Omega \quad \longrightarrow \text{unres.-scale eq.}$$

model dissipative effect on **fine** resolved scales       $\longleftarrow$  not solved for



# 3-Scale Velocity Separation

[Hughes et al. (2000), Collis (2001), Gravemeier (2003), ...]

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3 subproblems: coarse resolved + fine resolved + unresolved scales

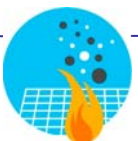
$$B_M(\overline{\mathbf{v}}^h; \overline{\mathbf{u}}^h + \mathbf{u}'^h, p^h) = (\overline{\mathbf{v}}^h, \mathbf{f})_\Omega \quad \longrightarrow \text{model. c.-s. eq.}$$

$$B_M(\mathbf{v}'^h; \overline{\mathbf{u}}^h + \mathbf{u}'^h, p^h) + (\varepsilon(\mathbf{v}'^h), 2\nu'_T \varepsilon(\mathbf{u}'^h)) = (\mathbf{v}'^h, \mathbf{f})_\Omega \quad \longrightarrow \text{model. f.-s. eq.}$$

Standard Smagorinsky model

$$\nu'_T = (C_S h)^2 |\varepsilon(\mathbf{u}'^h)|$$

model dissipative effect on **fine** resolved scales  $\longleftarrow$  not solved for



# Add PSPG Term: Circumventing LBB

[Hughes et al. (1986)]

Modeled coarse- and fine-scale momentum equation:

$$B_M(\bar{\mathbf{v}}^h; \bar{\mathbf{u}}^h + \mathbf{u}'^h, p^h) = (\bar{\mathbf{v}}^h, \mathbf{f})_\Omega$$

$$B_M(\mathbf{v}'^h; \bar{\mathbf{u}}^h + \mathbf{u}'^h, p^h) + (\varepsilon(\mathbf{v}'^h), 2\nu'_T \varepsilon(\mathbf{u}'^h)) = (\mathbf{v}'^h, \mathbf{f})_\Omega$$

Modeled continuity equation:

$$B_C(q^h; \mathbf{u}^h) + (\nabla q^h, \tau \mathcal{R}_M(\mathbf{u}^h, p^h)) = 0$$

Two modeling terms: fine-scale subgrid-viscosity term and PSPG term





# Practical Solution Strategies: Overview

	Explicit approach	Monolithic approach	
		$p$ -type scale separation	$h$ -type scale separation
FEM	Two-level FEM (RFB on small-scale level)	Hierarchical FEM (continuous/disc.)  $L_2$ -projection	<b>Multigrid scale separation</b> (project. and non-project. scale separation possible)
FVM			
FDM			Discrete smooth filters (non-projective)  Sampling + interpolation (applied in dynamic model)
SM		Spectral or sharp cutoff filter  Discrete smooth filters (non-projective)	

Source: V. Gravemeier, The variational multiscale method for laminar and turbulent flow, *Archives of Computational Methods in Engineering - State of the Art Reviews* 13 (2006) 249-324



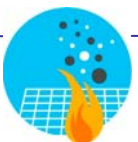
# Multigrid Approaches to (VM)LES

- Early geometric multigrid approaches to traditional LES, e.g., by Voke (1989) and Terracol *et al.* (2001) (also Sagaut *et al.* (2006))
- Volume-agglomeration method within finite volume / finite element formulation for scale separation in three-scale VMLES by Koobus and Farhat (2004)
  - challenging grid-based macro-cell agglomeration procedure via dual grid (Lallemand *et al.* (1992))
- Geometric multigrid method within finite volume formulation for scale separation in three-scale VMLES by Gravemeier (2006)
  - generation and maintenance of an additional grid required
- Related method by John & Kaya (2005), John *et al.* (2006):  $L_2$ -projection using two grids



# Outline

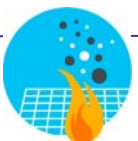
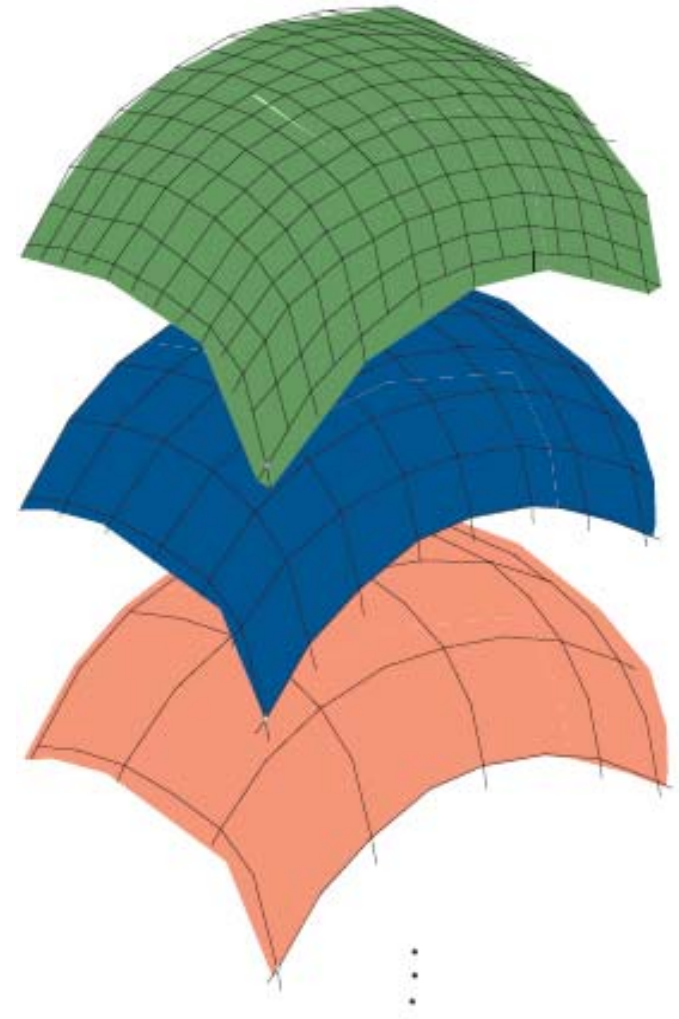
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# Multigrid Ingredients

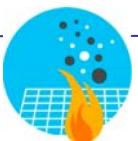
5 items are required:

- 1) A couple of grids or levels
- 2) A system of equations on each grid/level
- 3) Some approximate solution technique on each grid/level (relaxation)
- 4) A way to get from one grid/level to another (restriction / prolongation)
- 5) An algorithm or preconditioner



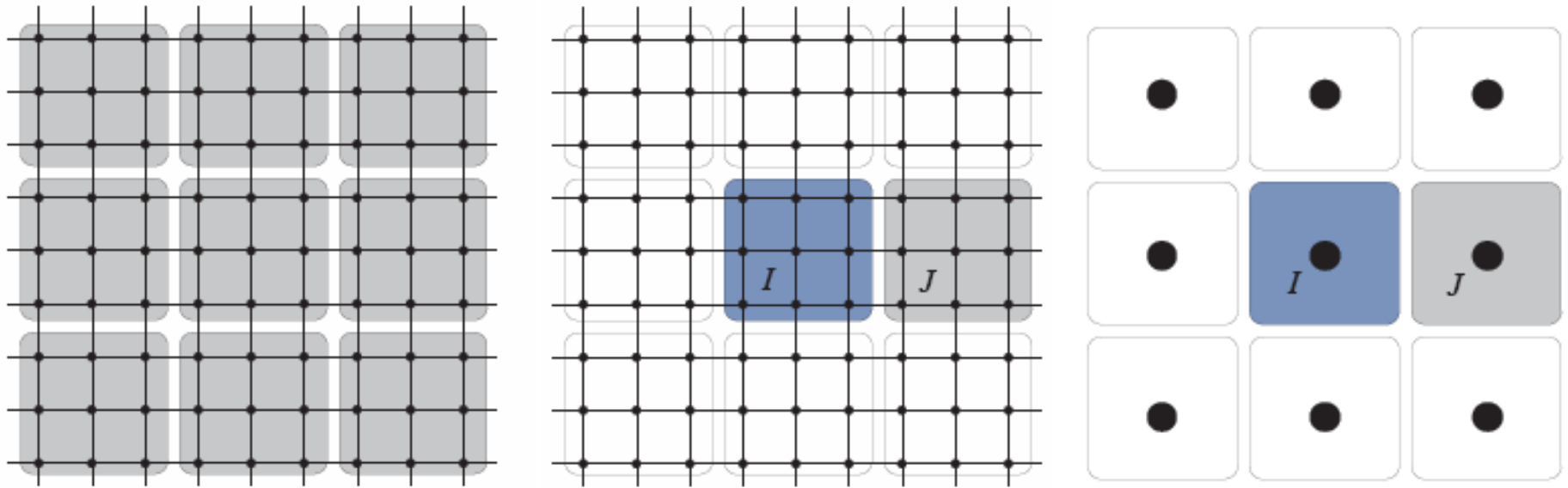
# Variants of Algebraic Multigrid (AMG) Methods

- Classical AMG ("Ruge-Stüben-AMG")  $\leftrightarrow$  Aggregation-based AMG
- Smoothed Aggregation AMG (SA-AMG) introduced by Vanek et al. (1996), optimal method for solution of elliptic problems, but inadequate for hyperbolic problems
- Plain Aggregation AMG (PA-AMG) better suited for hyperbolic problems, but sub-optimal when elliptic parts play a considerable role (e.g., in diffusion-dominated regions)
- Recent approach in form of a Petrov-Galerkin SA-AMG by Sala and Tuminaro (2008) for solving non-symmetric linear equation systems



# Plain and Smoothed Aggregation AMG

Aggregations due to connectivity/strength of connections of matrix entries:



(Tentative) prolongation operator matrix:  $\hat{\mathbf{P}}$

$\hat{P}_{iI} = 1$  if  $i$ -th entry in  $I$ -th aggregate, else  $\hat{P}_{iI} = 0$

Potential smoothing:  $\mathbf{P} = \mathbf{S}\hat{\mathbf{P}}$  with smoother  $\mathbf{S}$

Restriction:

$$\mathbf{R} = \mathbf{P}^T$$



# Reminder: Scale-Separated N-S Equations

Modeled coarse- and fine-scale momentum equation:

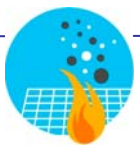
$$B_M(\bar{\mathbf{v}}^h; \bar{\mathbf{u}}^h + \mathbf{u}'^h, p^h) = (\bar{\mathbf{v}}^h, \mathbf{f})_\Omega$$

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Modeled continuity equation:

$$B_C(q^h; \mathbf{u}^h) + (\nabla q^h, \tau \mathcal{R}_M(\mathbf{u}^h, p^h)) = 0$$

Two modeling terms: fine-scale subgrid-viscosity term and PSPG term



# Multigrid Scale-Separated N-S Equations

Multigrid scale separation:  
[Harten (1996)]

$$\mathbf{v} = \mathbf{v}^{3h} + \mathbf{v}^{\delta h} + \hat{\mathbf{v}} \quad \mathbf{u} = \underbrace{\mathbf{u}^{3h} + \mathbf{u}^{\delta h}}_{\mathbf{u}^h} + \hat{\mathbf{u}}$$

Modeled coarse- and fine-scale momentum equation:

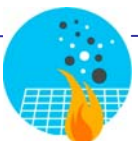
$$B_M(\mathbf{v}^{3h}; \mathbf{u}^{3h} + \mathbf{u}^{\delta h}, p^h) = (\mathbf{v}^{3h}, \mathbf{f})_\Omega$$

$$B_M(\mathbf{v}^{\delta h}; \mathbf{u}^{3h} + \mathbf{u}^{\delta h}, p^h) + (\varepsilon(\mathbf{v}^{\delta h}), 2\nu_T^{\delta h} \varepsilon(\mathbf{u}^{\delta h})) = (\mathbf{v}^{\delta h}, \mathbf{f})_\Omega$$

Modeled continuity equation:

$$\nu_T^{\delta h} = (C_S h)^2 |\varepsilon(\mathbf{u}^{\delta h})|$$

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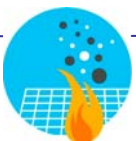




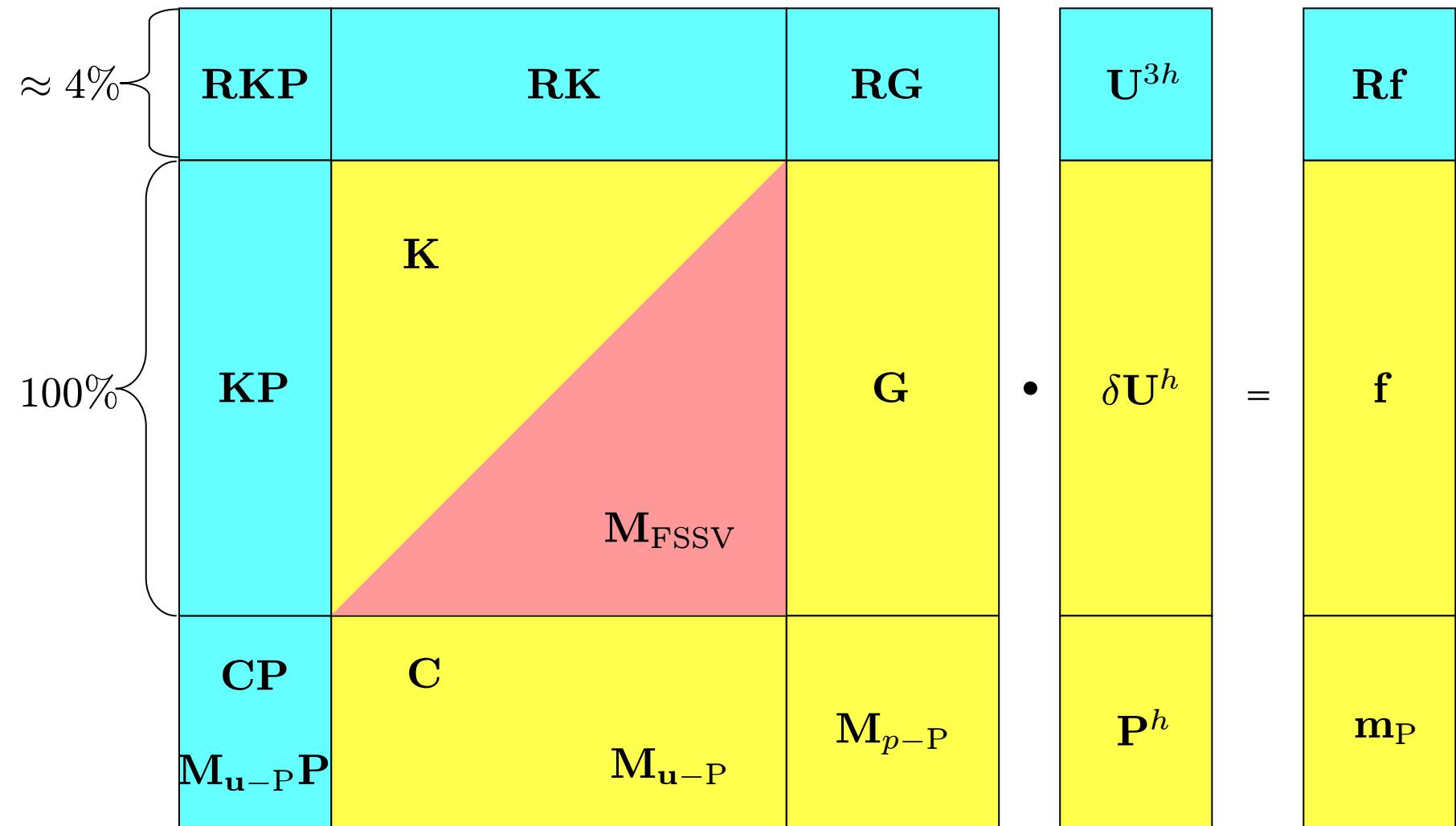
# PSPG-Stabilized N-S Matrix Formulation

$$\begin{array}{|c|c|} \hline \mathbf{K} & \mathbf{G} \\ \hline \mathbf{C} & \mathbf{M}_{p-P} \\ \hline \end{array} \cdot \begin{array}{|c|} \hline \mathbf{U}^h \\ \hline \mathbf{P}^h \\ \hline \end{array} = \begin{array}{|c|} \hline \mathbf{f} \\ \hline \mathbf{m}_P \\ \hline \end{array}$$

The diagram illustrates the PSPG-stabilized N-S matrix formulation. It shows a block matrix system where the unknowns are the velocity field  $\mathbf{U}^h$  and the pressure field  $\mathbf{P}^h$ . The matrix is composed of four blocks:  $\mathbf{K}$  (top-left),  $\mathbf{G}$  (top-right),  $\mathbf{C}$  (bottom-left), and  $\mathbf{M}_{p-P}$  (bottom-right). The right-hand side of the equation consists of two vectors:  $\mathbf{f}$  (top) and  $\mathbf{m}_P$  (bottom).

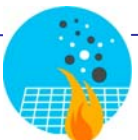


# Extended AVM<sup>3</sup> Formulation



# Remarks

- Extended AVM<sup>3</sup> formulation based on plain aggregation AMG: projective scale separation into coarse and fine (velocity) scales purely algebraically without need for an additional discretization
- Restriction of subgrid-viscosity matrix to fine scales by simply omitting it in level-transfer process
- Based on “ML” multigrid software package by Sandia NL, development of routine for generation of level-transfer operator matrices
- Multigrid solvers may beneficially exploit *a priori* separation of linear equation system into blocks containing different scales
  - Future work!
- Here: development and use of analogous re-condensed system, solving linear equation system using “standard” AMG solver



# Re-Condensed AVM<sup>3</sup> Formulation

Generate scale-separating matrix:  $\mathbf{S} = \mathbf{P}\mathbf{R}$

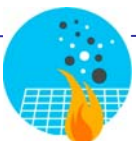
$$\begin{bmatrix} \mathbf{K} & \mathbf{G} \\ \mathbf{C} & \mathbf{M}_{p-P} \end{bmatrix} \cdot \begin{bmatrix} \mathbf{U}^h \\ \mathbf{P}^h \end{bmatrix} = \begin{bmatrix} \mathbf{f} \\ \mathbf{m}_P \end{bmatrix}$$

The matrix  $\mathbf{K}$  is partitioned into a yellow upper triangle and a pink lower triangle. The pink lower triangle contains the block matrix  $[\mathbf{I} - \mathbf{S}] \mathbf{M}_{\text{FSSV}} [\mathbf{I} - \mathbf{S}]$ . The matrix  $\mathbf{C}$  is labeled  $\mathbf{M}_{u-P}$  at the bottom right.



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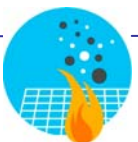


# Analysis of Scale Separation: 1D Model Problem

- Understand properties of scale separation from model equation (here already in variational FE formulation):

$$(v^h, \partial_t u^h)_\Omega + (\partial_x \delta v^h, \partial_x \delta u^h)_\Omega = 0$$

- Uniform discretization, periodic boundary conditions
- Linear finite elements
- Represents linearized, constant-coefficient model



# ODE system

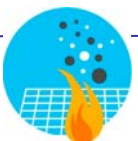
- 1D model gives discrete ODE system:

$$\frac{d}{dt} \mathbf{M} \mathbf{U}^h = [\mathbf{I} - \mathbf{S}] \mathbf{K}_{\text{diff}} [\mathbf{I} - \mathbf{S}] \mathbf{U}^h$$

- Also investigated: “one-sided” projection (computational efficiency)

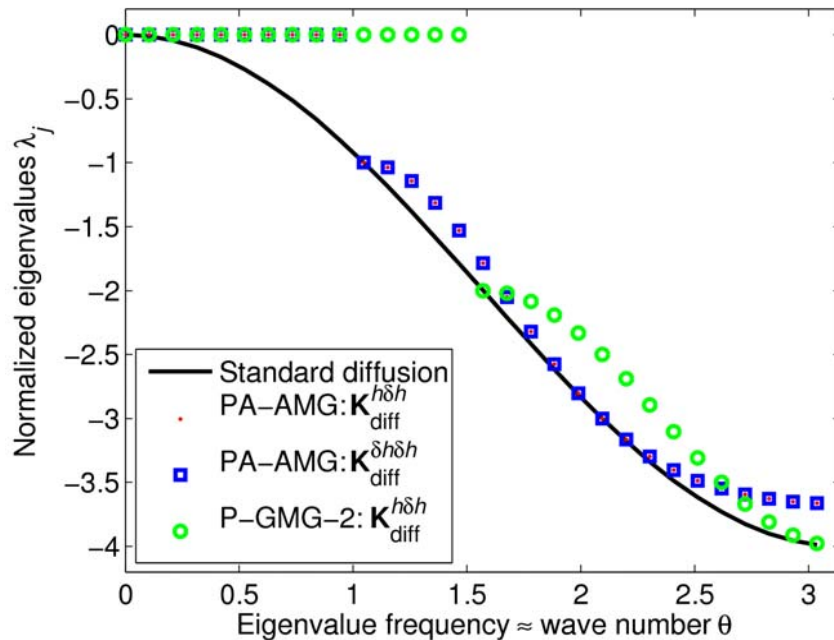
$$\frac{d}{dt} \mathbf{M} \mathbf{U}^h = \mathbf{K}_{\text{diff}} [\mathbf{I} - \mathbf{S}] \mathbf{U}^h$$

- Compare operators for  $\mathbf{K}_{\text{diff}}$  for various scale separations:
  - PA—AMG
  - SA—AMG
  - projective/smoothed geometric multigrid (P/S-GMG-2)
- Include comparison to standard (all-scale) subgrid-viscosity term

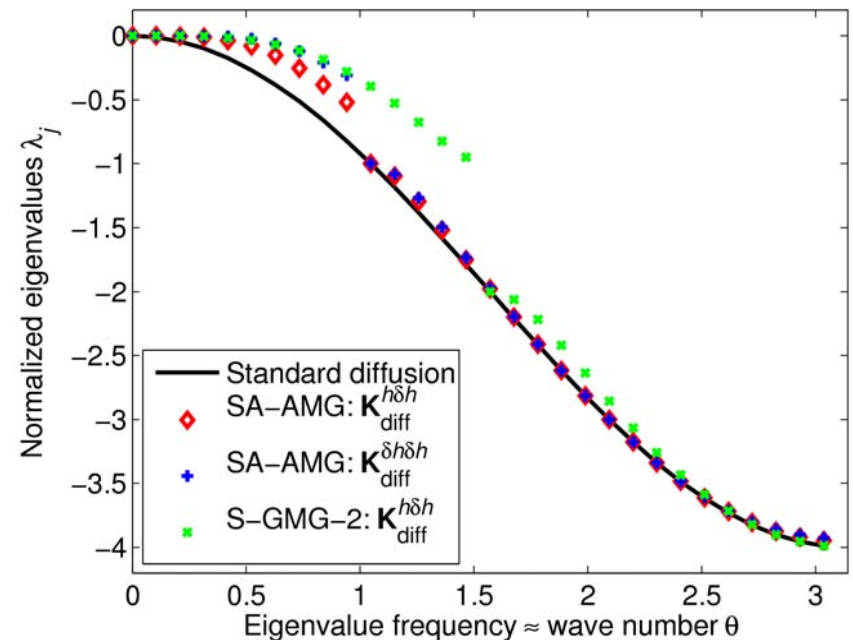


# Eigenvalues ( $h=1/60$ )

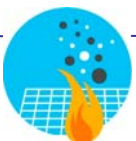
Eigenvalues govern temporal evolution of model:



projective scale separation



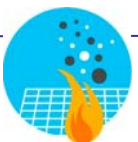
smoothed scale separation





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# The Competitors

(1) Traditional LES with dynamic Smagorinsky model (DSM) + PSPG

(2) Residual-Based Variational Multiscale Method (RBVMM)

Besides PSPG term, the following stabilization terms are included:

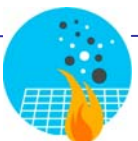
a) SUPG term

b) grad-div term (bulk viscosity term, LSIC,...)

c) cross-stress term

d) Reynolds-stress term

(according to Bazilevs *et al.* (2007), transient + viscous stab. terms omitted)



# Parameter Definitions

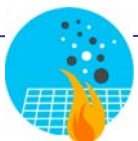
[Deardorff (1970), Franca and Valentin (2000), Barrenechea and Valentin (2002)]

Smagorinsky model parameter:  $C_S = 0.1$

SUPG, PSPG, cross-stress, and Reynolds-stress terms:

$$\tau_M = \frac{1}{\frac{1}{c_T \Delta t} \cdot \max(\xi_1, 1) + \frac{4\nu}{m_k h^2} \cdot \max(\xi_2, 1)} \quad \xi_1 = \frac{4\nu c_T \Delta t}{m_k h^2} \quad \xi_2 = \frac{m_k \|u^h\|_h}{2\nu}$$

grad-div term:  $\tau_C = \frac{\|u^h\|_h}{2} \cdot \min(\xi_2, 1) \quad \xi_2 = \frac{m_k \|u^h\|_h}{2\nu}$



# Overview: Turbulent Flow Problems

[Sagaut (2006)]

Homogeneous turbulent flows (0 directions of inhomogeneity)

Turbulent flows featuring 1 spatial direction of inhomogeneity

Turbulent flows featuring 2 spatial directions of inhomogeneity

Turbulent flows being completely inhomogeneous



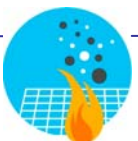
# Overview: Turbulent Flow Problems

Homogeneous turbulent flows (0 directions of inhomogeneity)

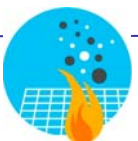
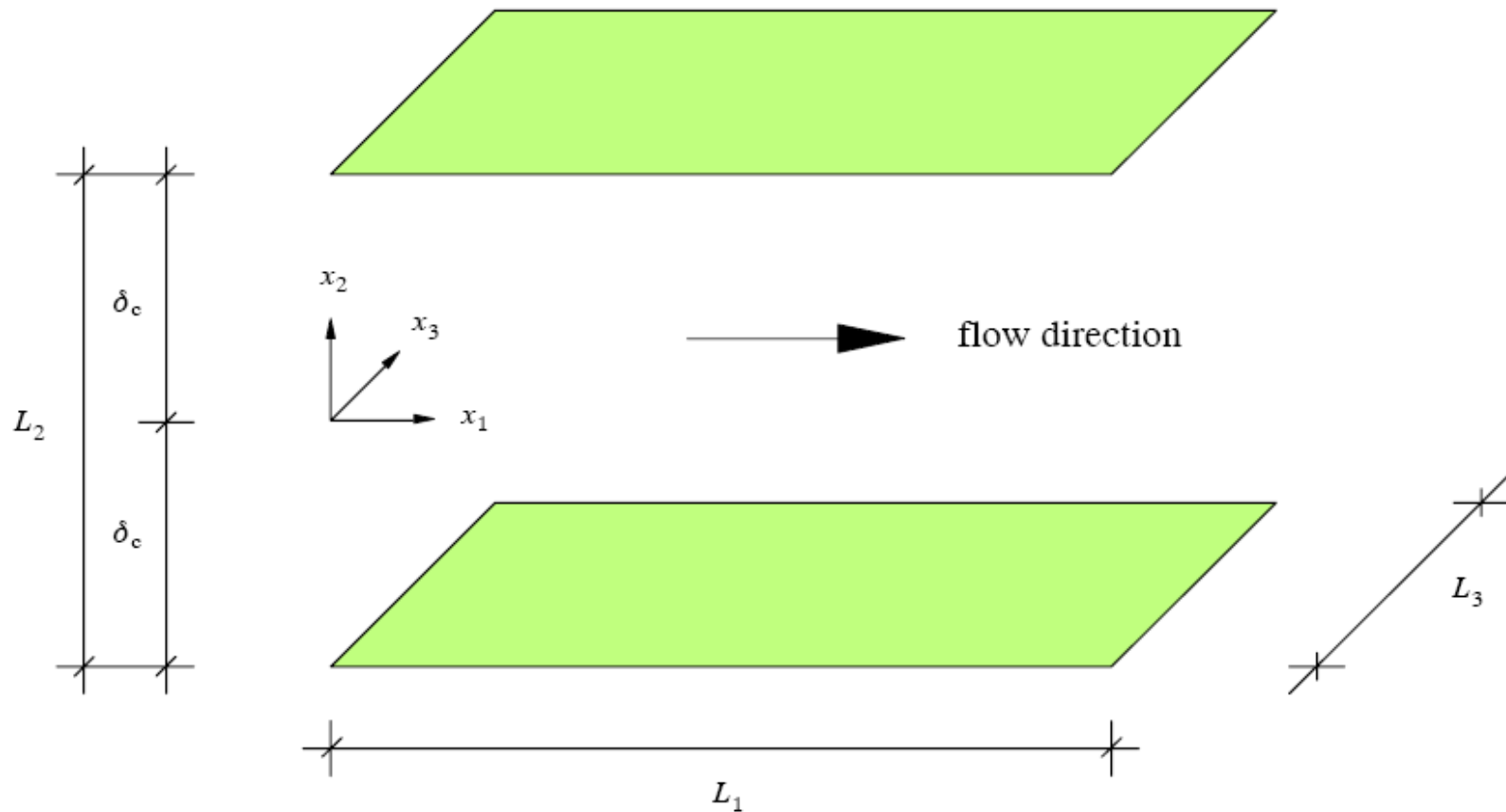
Turbulent flow in a channel

Turbulent flows featuring 2 spatial directions of inhomogeneity

Turbulent flows being completely inhomogeneous



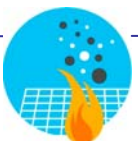
# Turbulent Flow in a Channel: Geometry



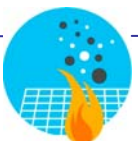
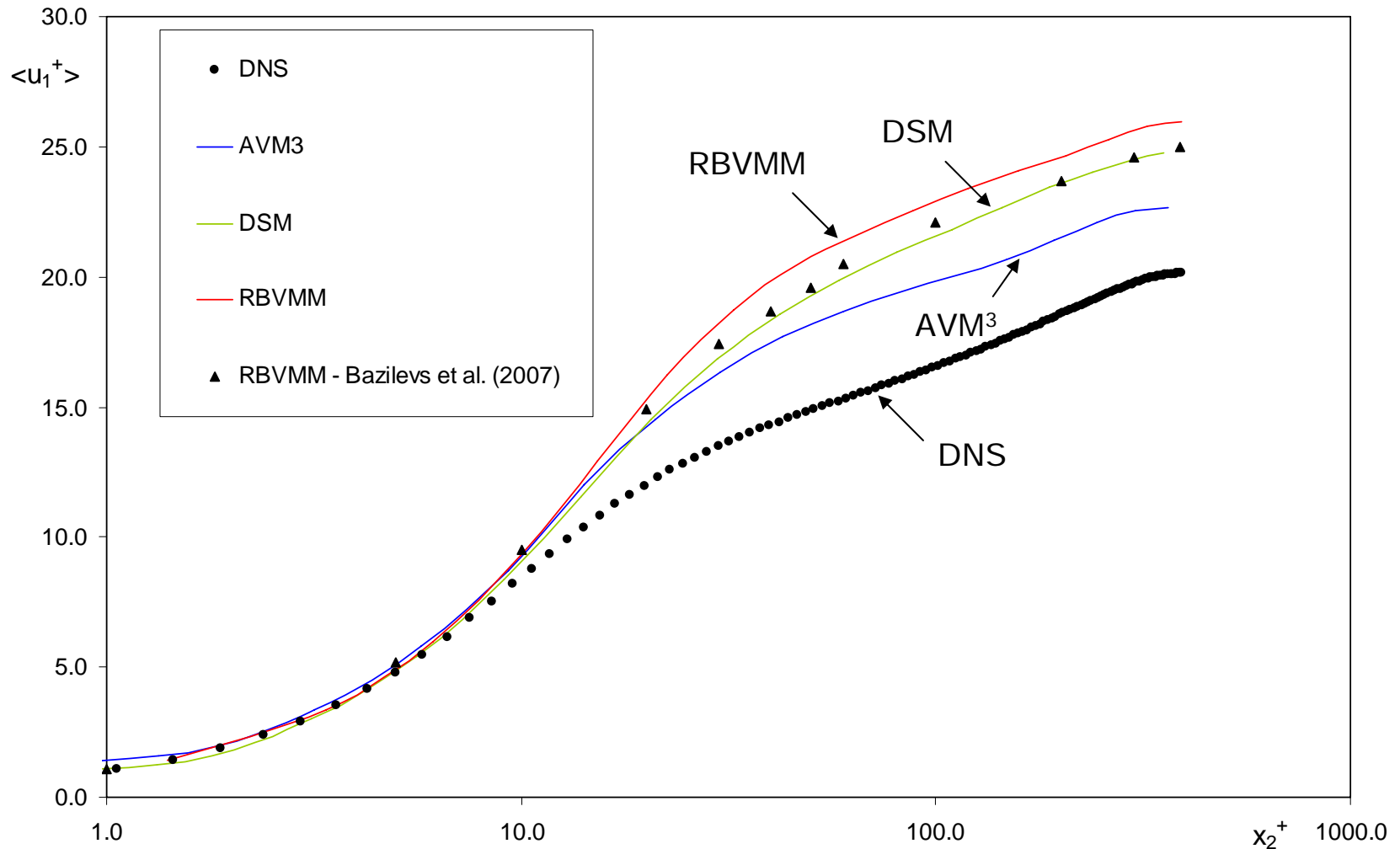
# Channel: Numerical Setup

- Reynolds number based on wall-shear velocity:  $Re_\tau = \frac{u_\tau \delta_c}{\nu} = 395$
- Channel dimensions:  $L_1 \times L_2 \times L_3 = 2\pi\delta_c \times \delta_c \times \frac{2}{3}\pi\delta_c$
- Generalized- $\alpha$  time integration scheme:  $\rho_\infty = 0.5$ ,  $\Delta t^+ = \frac{\Delta t u_\tau^2}{\nu} = 0.79$
- 32 linearly interpolated finite elements in each spatial direction
- hyperbolic refinement in wall-normal direction towards walls

$$\begin{array}{lll} h_1^+ = 77.56 & h_{2,\min}^+ = 1.32 & h_3^+ = 25.85 \\ & h_{2,\max}^+ = 67.78 & \end{array}$$

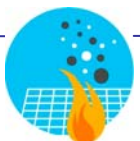
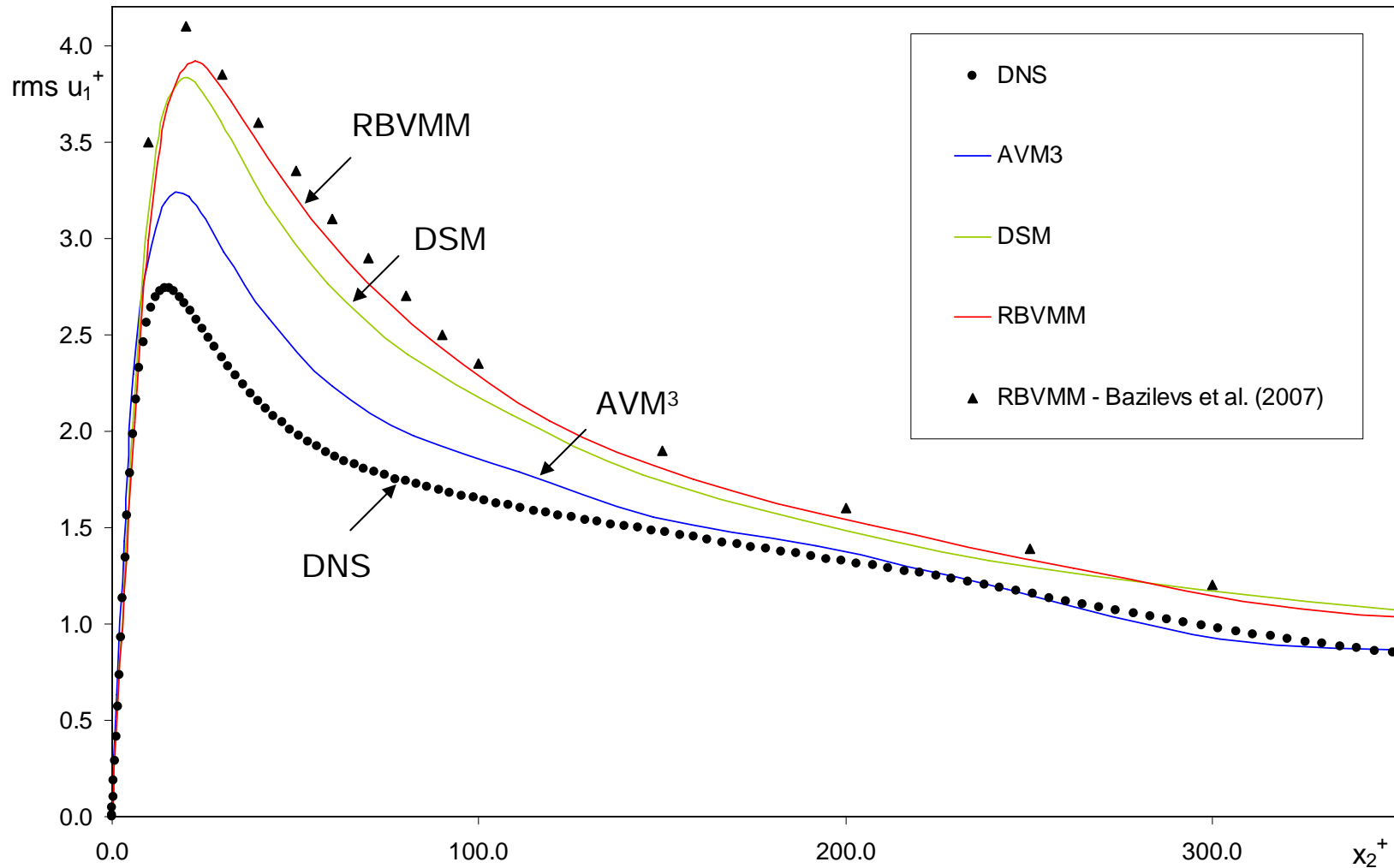


# Channel: Mean Streamwise Velocity

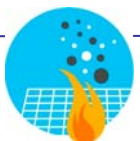
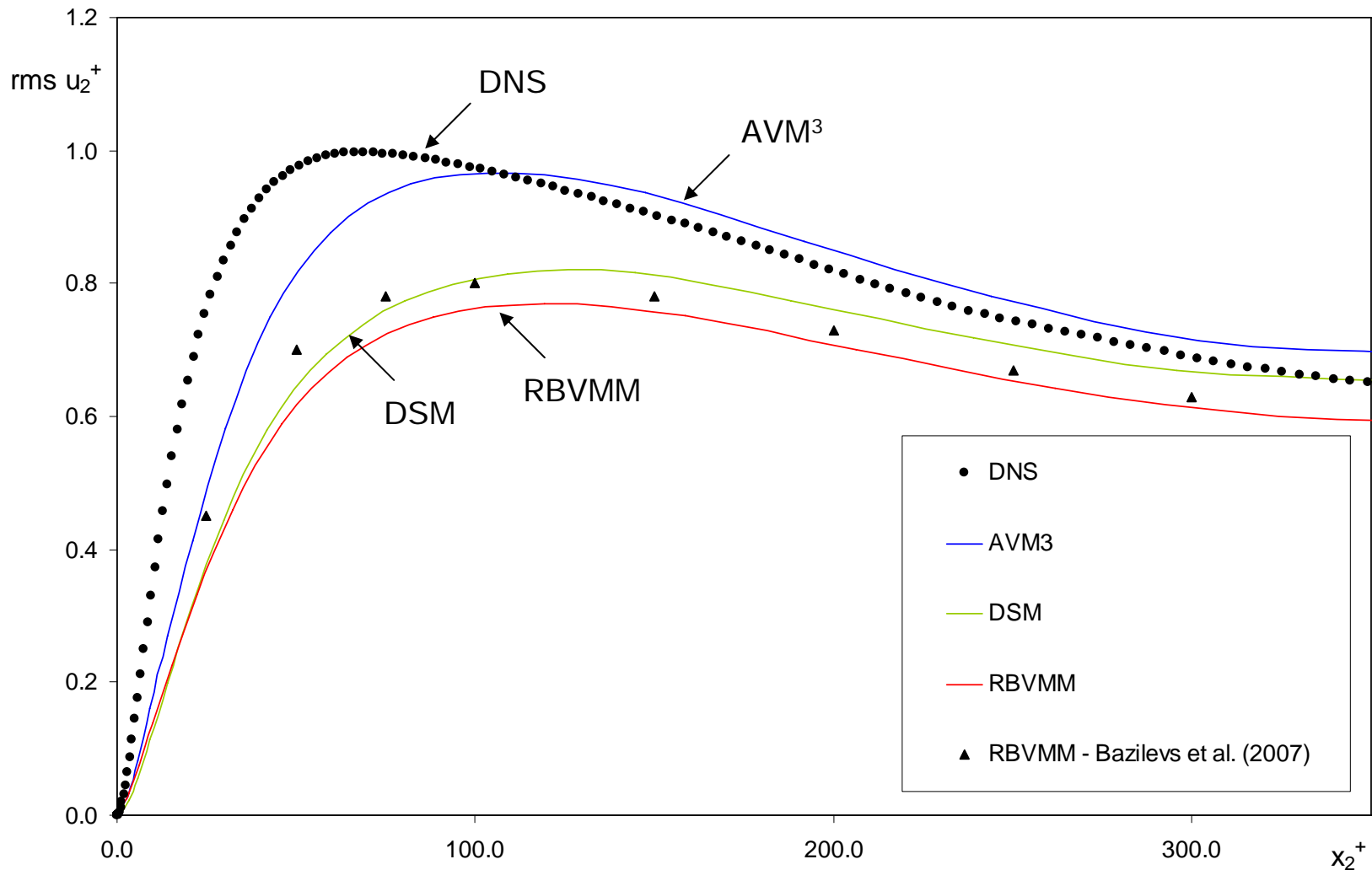




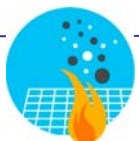
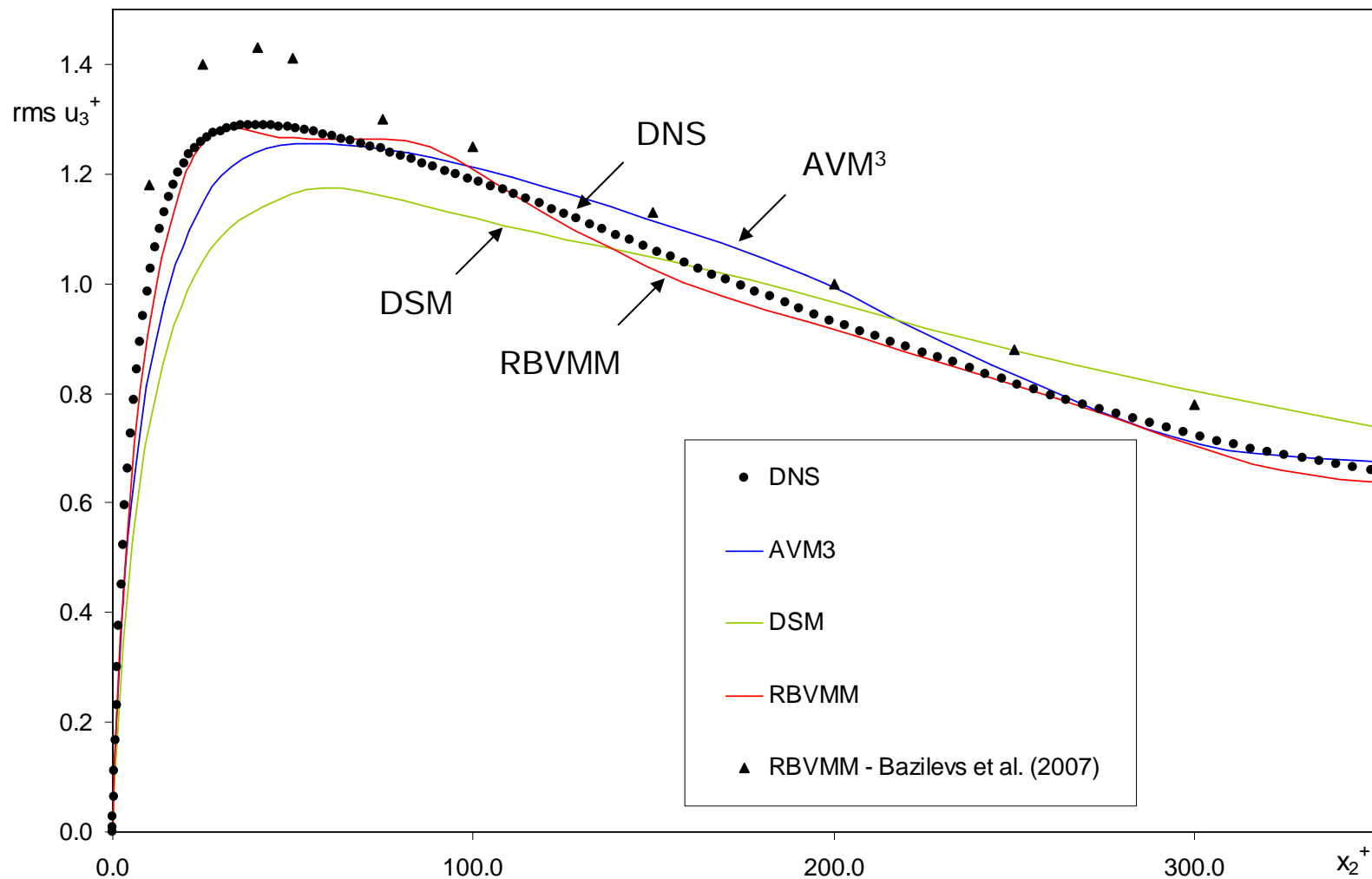
# Channel: RMS Streamwise Velocity



# Channel: RMS Wall-Normal Velocity



# Channel: RMS Spanwise Velocity



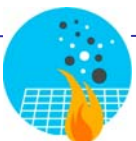
# Overview: Turbulent Flow Problems

Homogeneous turbulent flows (0 directions of inhomogeneity)

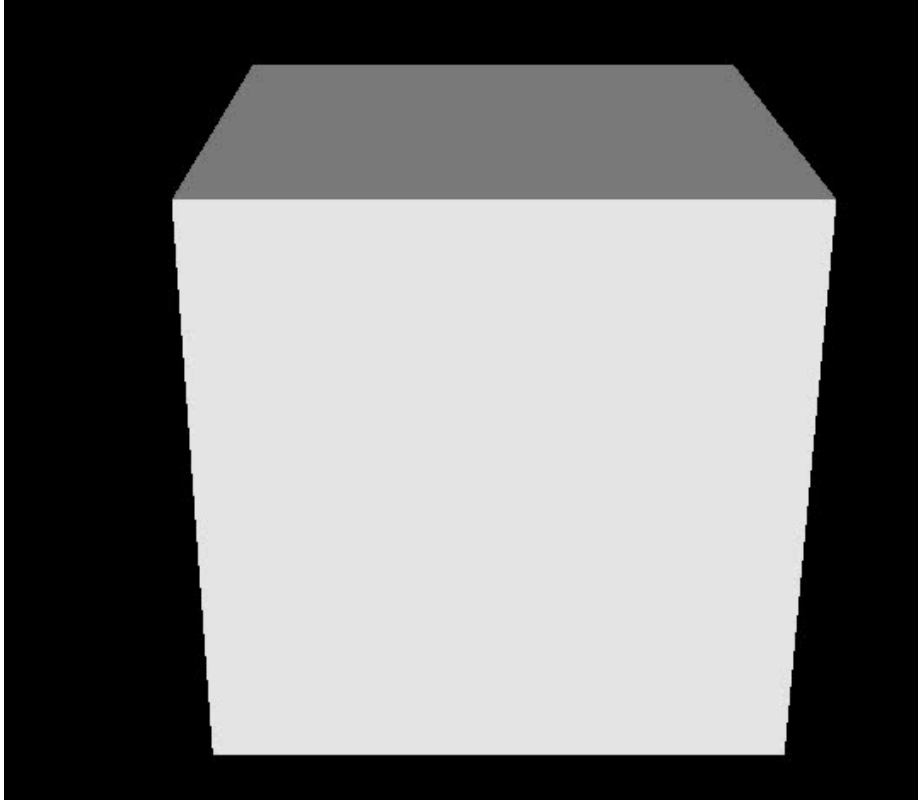
Turbulent flows featuring 1 spatial direction of inhomogeneity

Turbulent flows featuring 2 spatial directions of inhomogeneity

Turbulent recirculating flow in a lid-driven cavity



# Turbulent Flow in a Lid-Driven Cavity



Review of this flow problem:  
Shankar and Deshpande (2000)

Experimental study:  
Prasad and Koseff (1989)

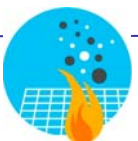
DNS study of Kolmogorov scales:  
Deshpande and Milton (1998)

Some LES studies: Zang et al. (1993), Bouffanais et al. (2007), ...

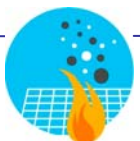
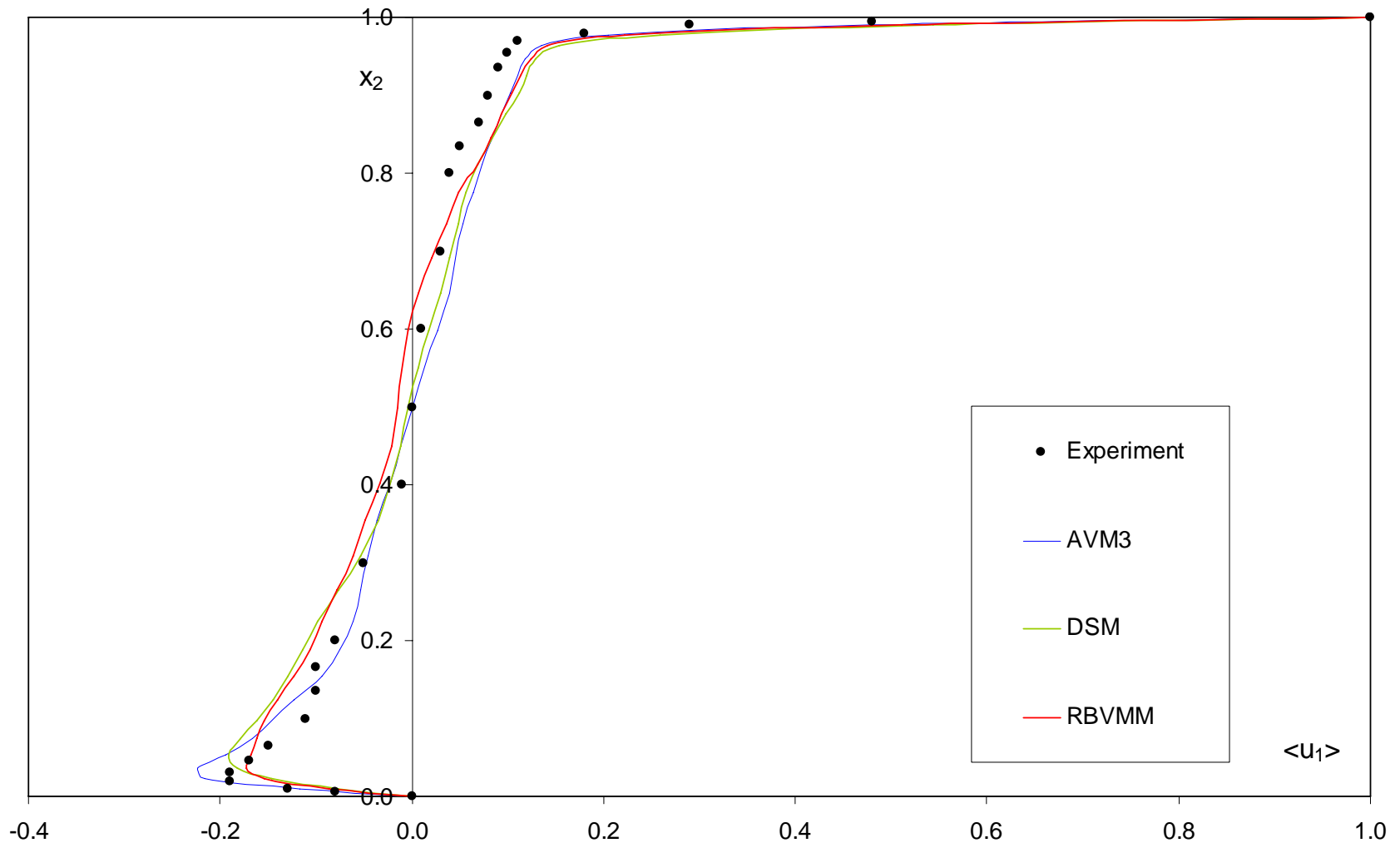


# Cavity: Numerical Setup

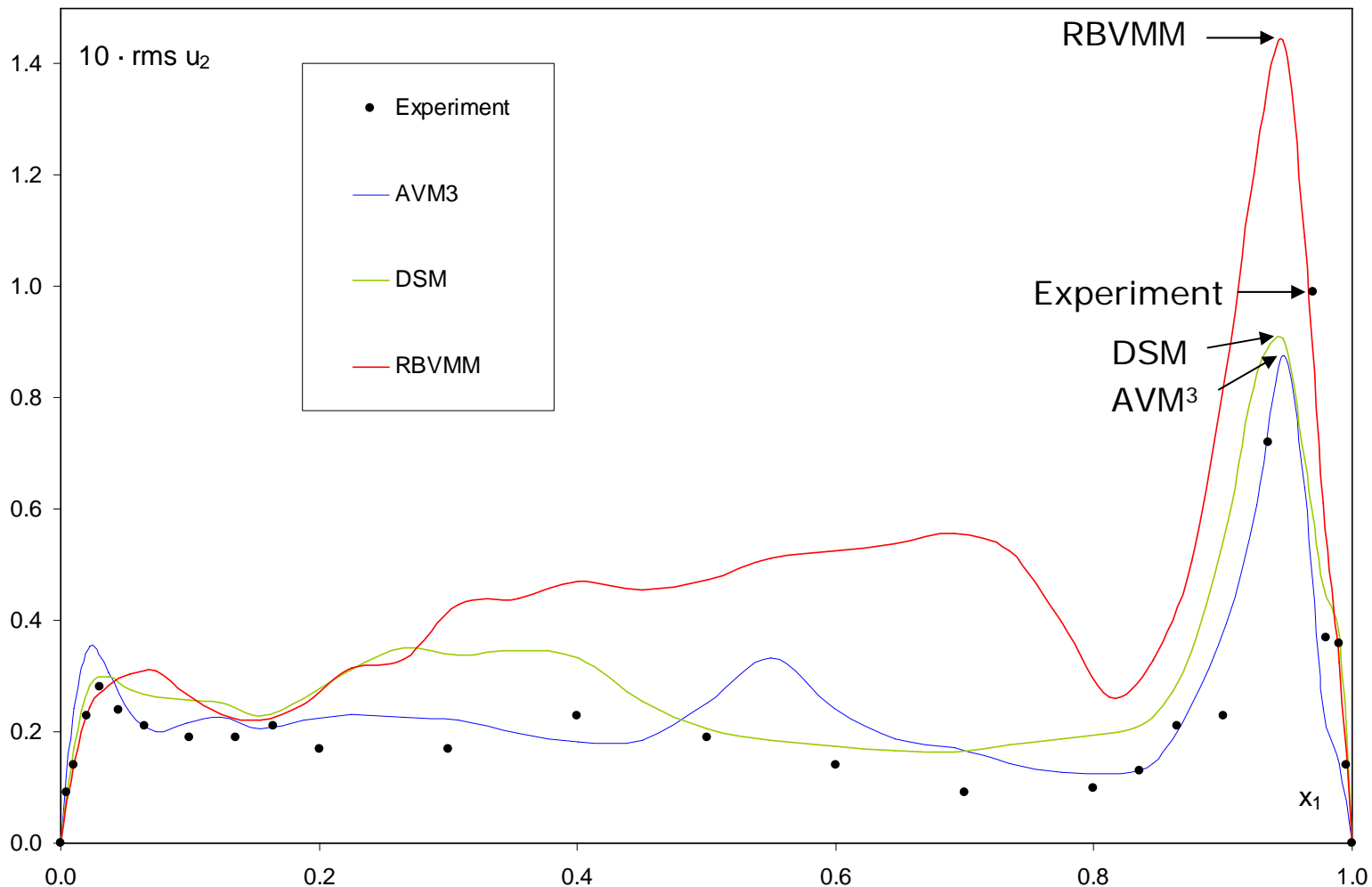
- Reynolds number based on top-lid velocity:  $Re = 10,000$
- Cavity with spanwise aspect ratio (SAR) 1.0:  $\Omega = [0, 1] \times [0, 1] \times [0, 1]$
- Crank-Nicolson time integration scheme:  $\Delta t = 0.1$
- Initial run time:  $5 T_{\text{cav}}$ , statistical evaluation period:  $5 T_{\text{cav}}$
- 32 linearly interpolated finite elements in each spatial direction
- refinement towards walls in  $x_1$ - and  $x_2$ -direction (min. length: 0.01)
- here: grad-div term added to AVM<sup>3</sup> and DSM for improv. convergence



# Cavity: Mean Velocity in $x_1$ -direction vs. $x_2$

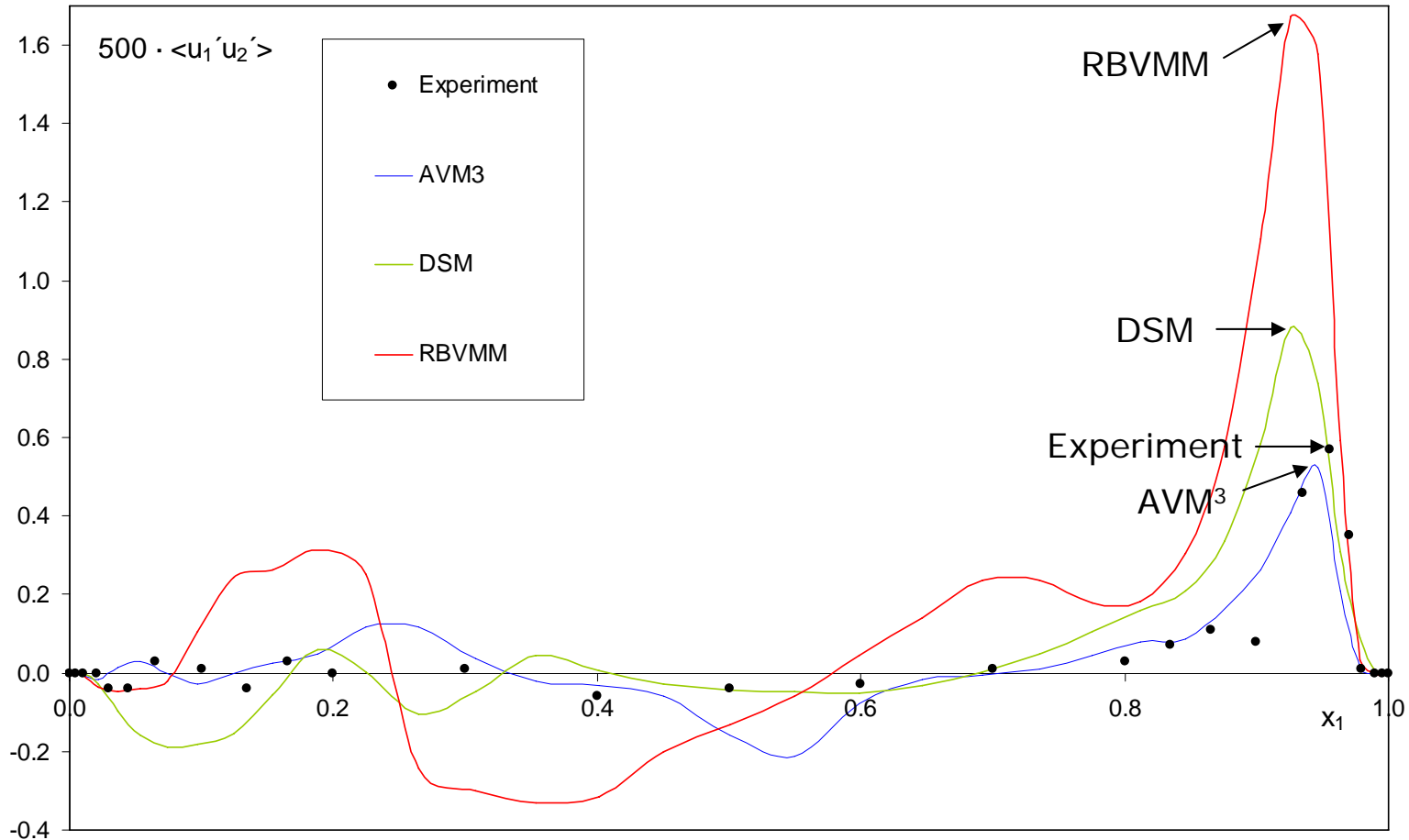


# Cavity: RMS Velocity in $x_2$ -direction vs. $x_1$





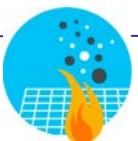
# Cavity: Reynolds-Stress Component 12 vs. $x_1$



# Computing Times

CPU Time	AVM <sup>3</sup>	RBVMM	DSM
Channel, $Re_\tau=180$ , $32^3$ elements	1.00	1.06	1.28
<b>Channel, <math>Re_\tau=395</math>, <math>32^3</math> elements</b>	1.00	1.30	1.16
Channel, $Re_\tau=590$ , $64^3$ elements	1.00	1.03	1.42
Cavity, $Re=3,200$ , $32^3$ elements	1.00	1.60	2.50
<b>Cavity, <math>Re=10,000</math>, <math>32^3</math> elements</b>	1.00	1.56	2.53

(normalized by computing time for AVM<sup>3</sup>)



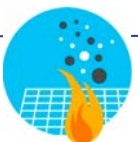
# Conclusions

- **Proposed method:** algebraic variational multiscale-multigrid method (AVM<sup>3</sup>) for three-scale VMLES of turbulent flows
- **Crucial features:** projective scale separation in a purely algebraic way using plain aggregation AMG level-transfer operators enables
  - efficient implementation
  - preservation of eigenvectors corresponding to low frequencies (standard models and smoothed scale separation damp low-frequency waves)
- **Computational evaluation:** comparison to residual-based VMLES and traditional dynamic Smagorinsky model for two (three) turbulent flow cases
- **Accuracy:** AVM<sup>3</sup> provides best results for all test cases, from mean flow values to highly sensitive Reynolds-stress components
- **Efficiency:** AVM<sup>3</sup> also computationally most efficient approach for all test cases



# Outlook

- Exploitation of “block-separated” extended AVM<sup>3</sup> matrix formulation for efficient solution approach
- Further investigation of potential combinations of residual-based two-scale and three-scale VMLES
- Grad-div term – angel or devil?
- Comprehensive computational evaluation for “turbulent obstacle course”
- Further steps towards LES of turbulent combustion



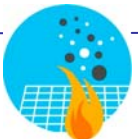
# Outlook: Turbulent Obstacle Course

Homogeneous turbulence is currently not of particular interest to us!

Turbulent flow in a channel

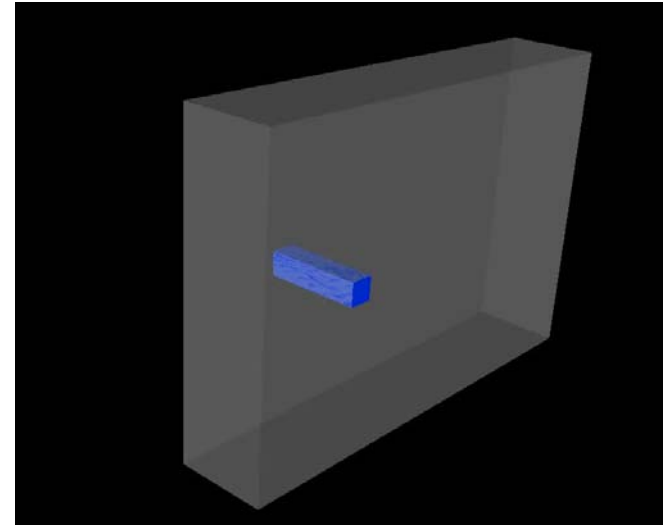
Outlook: Turbulent flow past a square-section cylinder

Turbulent recirculating flow in a lid-driven cavity



# Outlook: Turbulent Obstacle Course

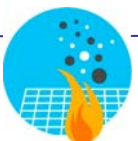
- Reynolds number:  $Re = 22,000$
- Flow domain and boundary conditions:  
Rodi *et al.* (1997): "Status of LES: Results of a Workshop"
- 103,680 elements; C-N:  $\Delta t = 0.075$



Outlook: Turbulent flow past a square-section cylinder



some early results



# Cylinder: Mean Streamwise Velocity

