

*EC*Math

for Mathematics Berlin

Weierstrass Institute for Applied Analysis and Stochastics

On p(x)-Laplace thermistor models describing electrothermal feedback in organic semiconductor devices

Matthias Liero

joint work with

Annegret Glitzky, Thomas Koprucki, Jürgen Fuhrmann (WIAS Berlin) Axel Fischer, Reinhard Scholz (IAPP, TU Dresden) Miroslav Bulìček (Charles University, Prague)

Introduction

Organic semiconductors

- Carbon-based materials conducting electrical current
- Used in smartphone and TV displays, photovoltaics, and lighting applications
- OLED: whole area emits light, flexible

Problem

- Luminance inhomogeneities emerge when operating at high currents
- Strong self-heating effects
- Counter-intuitive nonlinear phenomena

\Rightarrow PDE model needed!

Measurements by A. Fischer

Positive feedback loop in organic semiconductors

Organic semiconductors: Temperature-activated hopping transport of charge carriers

Positive feedback loop in organic semiconductors

Organic semiconductors: Temperature-activated hopping transport of charge carriers

p(x)-Laplace thermistor models \cdot ECMI \cdot Santiago de Compostela \cdot June 14, 2016 \cdot Page 2 (15)

Positive feedback loop in organic semiconductors

Organic semiconductors: Temperature-activated hopping transport of charge carriers

Fischer et al., Org. Elec., 2012

Zero-dimensional model with <u>Arrhenius law</u>, <u>non-Ohmic</u> current-voltage relation, and global heat balance

$$\begin{split} I(V,\mathbf{T}) &= I_{\text{ref}}F(\mathbf{T})\Big[\frac{V}{V_{\text{ref}}}\Big]^{\alpha} \qquad (\alpha \geq 1)\\ F(\mathbf{T}) &= \exp\left[-\frac{E_{\text{act}}}{k_{\text{B}}}\Big(\frac{1}{T} - \frac{1}{T_{\text{a}}}\Big)\right]\\ \frac{1}{\Theta_{\text{th}}}(\mathbf{T} - T_{\text{a}}) &= I(V,\mathbf{T}) \cdot V \end{split}$$

Thermistor behavior with regions of negative differential resistance Fischer et al. PRL, 2013

Inhomogeneities in large-area OLEDs

- OLEDs consist of various layers and have huge aspect ratios
- Optical transparent top electrode has large sheet resistance
- Sheet resistance leads to significant lateral potential drop

Spatially resolved models needed.

We consider elliptic system consisting of current-flow equation for electrostatic potential φ and heat equation for temperature T

$$-\nabla \cdot \left(\sigma(x, T, \nabla \varphi) \nabla \varphi\right) = 0$$
$$-\nabla \cdot \left(\lambda(x) \nabla T\right) = \eta(x) \sigma(x, T, \nabla \varphi) |\nabla \varphi|^2$$

We consider elliptic system consisting of current-flow equation for electrostatic potential φ and heat equation for temperature T

$$\begin{split} -\nabla\cdot\left(\sigma(x,\boldsymbol{T},\nabla\varphi)\nabla\varphi\right) &= 0\\ -\nabla\cdot\left(\lambda(x)\nabla\boldsymbol{T}\right) &= \eta(x)\sigma(x,\boldsymbol{T},\nabla\varphi)|\nabla\varphi|^2 \end{split}$$

with electrical conductivity $\sigma:\Omega\times\mathbb{R}\times\mathbb{R}^d\to[0,\infty)$ given by

$$\begin{split} \sigma(x, \mathbf{T}, \nabla \varphi) &= \sigma_0(x) F(x, \mathbf{T}) \Big[\frac{|\nabla \varphi|}{V_{\text{ref}} / \ell_{\text{ref}}} \Big]^{p(x) - 2} \\ F(x, \mathbf{T}) &= \exp \Big[-\frac{E_{\text{act}}(x)}{k_{\text{B}}} \Big(\frac{1}{\mathbf{T}} - \frac{1}{T_{\text{a}}} \Big) \Big] \end{split}$$

We consider elliptic system consisting of current-flow equation for electrostatic potential φ and heat equation for temperature T

$$\begin{split} -\nabla\cdot\left(\sigma(x,\boldsymbol{T},\nabla\varphi)\nabla\varphi\right) &= 0\\ -\nabla\cdot\left(\lambda(x)\nabla\boldsymbol{T}\right) &= \eta(x)\sigma(x,\boldsymbol{T},\nabla\varphi)|\nabla\varphi|^2 \end{split}$$

with electrical conductivity $\sigma:\Omega\times\mathbb{R}\times\mathbb{R}^d\to[0,\infty)$ given by

$$\sigma(x, \mathbf{T}, \nabla \varphi) = \sigma_0(x) F(x, \mathbf{T}) \left[\frac{|\nabla \varphi|}{V_{\text{ref}} / \ell_{\text{ref}}} \right]^{p(x) - 2}$$

$$F(x, \mathbf{T}) = \exp\left[-\frac{E_{\mathsf{act}}(x)}{k_{\mathsf{B}}} \left(\frac{1}{\mathbf{T}} - \frac{1}{T_{\mathsf{a}}}\right)\right]^{-1}$$

PDE model can be motivated from equivalent circuit model s.t. finite-volume discretization of PDE system correspond to Kirchhoff's circuit rules $V_{0} = \underbrace{\begin{bmatrix} \mathbf{R}_{0} & \mathbf{R}_{0} \\ \mathbf{R}_{0} \\ \mathbf{R}_{0} & \mathbf{R}_{0}$

(see Fischer et al. 2014, ~> talk by A. Fischer, Wed)

p(x)-Laplace thermistor models \cdot ECMI \cdot Santiago de Compostela \cdot June 14, 2016 \cdot Page 4 (15)

$$-\nabla \cdot \left(\sigma_0(x)F(x,T)|\nabla \varphi|^{p(x)-2}\nabla \varphi\right) = 0$$

$$-\nabla \cdot \left(\lambda(x)\nabla T\right) = \eta(x)\sigma_0(x)F(x,T)|\nabla \varphi|^{p(x)}$$

Mixed boundary conditions

$$\begin{split} \varphi &= \varphi^D \quad \text{on } \Gamma_D \qquad \sigma(x,T,\nabla\varphi)\nabla\varphi \cdot \nu = 0 \quad \text{on } \Gamma_N \\ &-\lambda(x)\nabla T \cdot \nu = \kappa(x)(T-T_{\mathsf{a}}) \quad \text{on } \Gamma := \partial\Omega \end{split}$$

$$-\nabla \cdot \left(\sigma_0(x)F(x,T)|\nabla \varphi|^{p(x)-2}\nabla \varphi\right) = 0$$

$$-\nabla \cdot \left(\lambda(x)\nabla T\right) = \eta(x)\sigma_0(x)F(x,T)|\nabla \varphi|^{p(x)}$$

Mixed boundary conditions

$$\begin{split} \varphi &= \varphi^D \quad \text{on } \Gamma_D \qquad \sigma(x, T, \nabla \varphi) \nabla \varphi \cdot \nu = 0 \quad \text{on } \Gamma_N \\ &-\lambda(x) \nabla T \cdot \nu = \kappa(x) (T - T_{\mathsf{a}}) \quad \text{on } \Gamma := \partial \Omega \end{split}$$

Properties

- Current-flow equation is of p(x)-Laplacian type
- Abrupt change of p(x) between materials:

Exponent p(x) describes non-Ohmic behavior of materials, p(x)=2 in electrodes (Ohmic) and p(x)>2 in organic materials (e.g. p(x)=9.7)

For
$$abla arphi \in L^{p(x)}(\Omega)^d$$
, Joule heat term in general only in L^1

$$-\nabla \cdot \left(\sigma_0(x)F(x,T)|\nabla \varphi|^{p(x)-2}\nabla \varphi\right) = 0$$

$$-\nabla \cdot \left(\lambda(x)\nabla T\right) = \eta(x)\sigma_0(x)F(x,T)|\nabla \varphi|^{p(x)}$$

Mixed boundary conditions

$$\begin{split} \varphi &= \varphi^D \quad \text{on } \Gamma_D \qquad \sigma(x, \mathbf{T}, \nabla \varphi) \nabla \varphi \cdot \nu = 0 \quad \text{on } \Gamma_N \\ &-\lambda(x) \nabla \mathbf{T} \cdot \nu = \kappa(x) (\mathbf{T} - T_{\mathsf{a}}) \quad \text{on } \Gamma := \partial \Omega \end{split}$$

- (i) Effective elec. conductivity $\sigma_0 \in L^{\infty}(\Omega)$ s.t. $0 < \underline{\sigma_0} \le \sigma_0 \le \overline{\sigma_0}$ a.e. in Ω
- (ii) Thermal conductivity $\lambda \in L^{\infty}_{+}(\Omega)$ s.t. $0 < \lambda_{*} \leq \lambda \leq \overline{\lambda_{*}} < \infty$ a.e. in Ω
- (iii) Activation energy $E_{act} \in L^{\infty}_{+}(\Omega)$
- (iv) Heat transfer coefficient $\kappa \in L^{\infty}_{+}(\Omega), \int_{\Gamma} \kappa(x) d\Gamma > 0$
- (v) Light-outcoupling factor $\eta\in L^\infty(\Omega),$ $\eta\in[0,1]$ a.e. in Ω
- (vi) Ambient temperature $T_a > 0$ is constant
- (vii) Dirichlet data $\varphi_D \in W^{1,\infty}(\Omega)$
- (viii) Power-law exponent $x \mapsto p(x)$ is measurable and

$$1 < p_{-} := \operatorname{ess\,inf}_{x \in \Omega} p(x) \le \operatorname{ess\,sup}_{x \in \Omega} p(x) =: p_{+} < \infty$$

Theorem (Bulíček-Glitzky-L. 2016 a)

There exists a weak solution to the coupled system

$$\begin{array}{ll} (\textit{Current flow}) & & -\nabla\cdot\left(\sigma(x,T,|\nabla\varphi|)\nabla\varphi\right) = 0 \\ (\textit{Heat flow}) & & & -\nabla\cdot\left(\lambda(x)\nabla T\right) \\ & & & -\nabla\cdot\left(\lambda(x)\nabla T\right) \\ & & = \eta(x)\sigma(x,T,|\nabla\varphi|)|\nabla\varphi|^2 \end{array}$$

with

$$\begin{split} \varphi &= \varphi^D \quad \text{on } \Gamma_D \qquad \sigma(x,T,\nabla\varphi) \nabla \varphi \cdot \nu = 0 \quad \text{on } \Gamma_N \\ &\quad -\lambda(x) \nabla T \cdot \nu = \kappa(x) (T-T_{\mathsf{a}}) \quad \text{on } \Gamma := \partial \Omega \end{split}$$

where $\varphi \in W^{1,p(x)}(\Omega)$ and $T \in W^{1,q}(\Omega)$ with $1 \leq q < d/(d-1)$, and

$$\operatorname{ess\,inf} \varphi^D \leq \varphi(x) \leq \operatorname{ess\,sup} \varphi^D, \qquad T \geq T_{\mathrm{a}} \quad \textit{a.e. in } \Omega.$$

Note: More general constitutive equations for the electrical current can be considered.

1. For $\varepsilon > 0$, introduce regularization

$$f_{\varepsilon}(x,T,\nabla\varphi):=\eta(x)\frac{\sigma(x,T,\nabla\varphi)|\nabla\varphi|^2}{1+\varepsilon\sigma(x,T,\nabla\varphi)|\nabla\varphi|^2}\leq \frac{1}{\varepsilon}$$

- Solve regularized problem via Galerkin approximation (use strict monotonicity of current law)
- 3. For solutions $(\varphi_{\varepsilon}, T_{\varepsilon})$ of regularized problem derive uniform estimates by testing weak formulation with suitable functions, e.g. $\tilde{T} = T_{\varepsilon}^{-\delta}$ ($\delta \in (0, 1)$)

$$\|\nabla \varphi_{\varepsilon}\|_{p(\cdot)} \leq C, \qquad \|T_{\varepsilon}\|_{W^{1,q}} \leq C(q), \quad \text{where } q \in \left[1, \frac{d}{d-1}\right)$$

4. Pass to the limit $\varepsilon \to 0$ in the weak formulation and identify limits exploiting monotonicity again

Numerics for thermistor scheme

Lnibriz

Our numerical scheme is based on a hybrid finite element/volume approach, see also Bradji–Herbin 2008

$$\int_{K} \nabla \cdot \mathbf{J} \, \mathrm{d}x = \sum_{L|K} \int_{s_{KL}} \mathbf{J} \cdot \mathbf{n}_{KL} \, \mathrm{da}$$
$$\approx \sum_{L|K} |s_{KL}| J_{KL}$$

Finite volume scheme

Construct approximation J_{KL} of normal flux $\mathbf{J} \cdot \mathbf{n}_{KL}$

Numerics for thermistor scheme

Our numerical scheme is based on a hybrid finite element/volume approach, see also Bradji–Herbin 2008

$$\int_{K} \nabla \cdot \mathbf{J} \, \mathrm{d}x = \sum_{L|K} \int_{s_{KL}} \mathbf{J} \cdot \mathbf{n}_{KL} \, \mathrm{da}$$
$$\approx \sum_{L|K} |s_{KL}| J_{KL}$$

Finite volume scheme

Construct approximation J_{KL} of normal flux $\mathbf{J} \cdot \mathbf{n}_{KL}$

Heat equation

$$\int_{K} \nabla \cdot (\lambda(x) \nabla T) \, \mathrm{d}x \approx \sum_{L|K} |s_{KL}| \lambda_{KL} \frac{T_L - T_K}{|x_L - x_K|}$$

Problem: In current-flow equation the conductivity σ depends not only on normal component $\nabla \varphi \cdot \mathbf{n}$ on Voronoi surface but also on tangential components.

Given nodal values $\{\varphi_K\}$ construct P1 finite element interpolant $\hat{\varphi}_T$

Lnibriz

Problem: In current-flow equation the conductivity σ depends not only on normal component $\nabla \varphi \cdot \mathbf{n}$ on Voronoi surface but also on tangential components.

Given nodal values $\{\varphi_K\}$ construct P1 finite element interpolant $\hat{\varphi}_T$

Current-flux approximation (for same material region)

$$\begin{split} \int_{K} \nabla \cdot \left(\sigma(x, T, |\nabla \varphi|) \nabla \varphi \right) \mathrm{d}x &= \sum_{L|K} \int_{s_{KL}} \sigma_0(x) F(x, T) |\nabla \varphi|^{p(x) - 2} \nabla \varphi \cdot \mathbf{n} \, \mathrm{d}a \\ &\approx \sum_{L|K} |s_{KL}| F_{s_{KL}}(T_{KL}) \left| \overline{\nabla \varphi_{\mathcal{T}}} \right|^{p_{s_{KL}} - 2} \frac{\varphi_L - \varphi_K}{|x_K - x_L|} \end{split}$$

Lnibriz

Problem: In current-flow equation the conductivity σ depends not only on normal component $\nabla \varphi \cdot \mathbf{n}$ on Voronoi surface but also on tangential components.

Given nodal values $\{\varphi_K\}$ construct P1 finite element interpolant $\hat{\varphi}_T$

Current-flux approximation (for same material region)

$$\int_{K} \nabla \cdot \left(\sigma(x, T, |\nabla \varphi|) \nabla \varphi \right) \mathrm{d}x = \sum_{L|K} \int_{s_{KL}} \sigma_0(x) F(x, T) |\nabla \varphi|^{p(x) - 2} \nabla \varphi \cdot \mathbf{n} \, \mathrm{d}a$$
$$\approx \sum_{L|K} |s_{KL}| F_{s_{KL}}(T_{KL}) \left| \overline{\nabla \varphi_{\mathcal{T}}} \right|^{p_{s_{KL}} - 2} \frac{\varphi_L - \varphi_K}{|x_K - x_L|}$$

- Averaging of |
 abla arphi| is necessary for stable schemes on general grids
- At material interface no averaging is performed to avoid artificial lateral diffusion
- Needs boundary conforming Delaunay grids

Simulation study for p(x)-Laplace equation $-\nabla\cdot(|\nabla u|^{p(x)-2}\nabla u)=1$ with Dirichlet boundary conditions

Problem: In voltage-controlled simulations, solutions have to jump into high conductance state, current-controlled simulations numerically unstable

Problem: In voltage-controlled simulations, solutions have to jump into high conductance state, current-controlled simulations numerically unstable

- Simulation of IV curves via numerical path following methods
- Solve extended system for (φ, T, V) with V applied voltage
- Predictor-corrector scheme with step-size control

Problem: In voltage-controlled simulations, solutions have to jump into high conductance state, current-controlled simulations numerically unstable

- Simulation of IV curves via numerical path following methods
- Solve extended system for (φ, T, V) with V applied voltage
- Predictor-corrector scheme with step-size control

Recall: Counter-intuitive phenomena in large-area OLEDs

- High sheet resistance of optical transparent electrode cannot explain saturation of current
- degradation of material can also be excluded due to lower temperature center of panel
- Effect is caused by interplay between S-NDR and heat conduction

Pattern formation in OLEDs induced by operation modes propagating through device

Operation modes are characterized by

local differential resistance

$$\frac{\mathrm{d}V_x}{\mathrm{d}I_x} = \left(\frac{\mathrm{d}V_x}{\mathrm{d}I_{\mathsf{tot}}}\right) \left(\frac{\mathrm{d}I_x}{\mathrm{d}I_{\mathsf{tot}}}\right)^{-1}$$

 $I_{\rm tot}$ total current

- I_x local current through stack
- V_x local voltage drop

| Modes | for | $I_{\rm tot} \uparrow$ |
|---------------|------------------|------------------------|
| Normal | $V_x \uparrow$ | $I_x \uparrow$ |
| S-NDR | $V_x \downarrow$ | $I_x \uparrow$ |
| Switched-back | $V_x \downarrow$ | $I_x \downarrow$ |
| N-NDR | $V_x \uparrow$ | $I_x \downarrow$ |

Pattern formation in OLEDs induced by operation modes propagating through device

Operation modes are characterized by local differential resistance

$$\frac{\mathrm{d}V_x}{\mathrm{d}I_x} = \left(\frac{\mathrm{d}V_x}{\mathrm{d}I_{\mathsf{tot}}}\right) \left(\frac{\mathrm{d}I_x}{\mathrm{d}I_{\mathsf{tot}}}\right)^{-1}$$

 $I_{\rm tot}$ total current

- I_x local current through stack
- V_x local voltage drop

| Modes | for | $I_{\rm tot}\uparrow$ |
|---------------|------------------|-----------------------|
| Normal | $V_x \uparrow$ | $I_x \uparrow$ |
| S-NDR | $V_x \downarrow$ | $I_x \uparrow$ |
| Switched-back | $V_x \downarrow$ | $I_x \downarrow$ |
| N-NDR | $V_x \uparrow$ | $I_x \downarrow$ |

For sufficiently high applied currents center of panel is switched back.

- Introduced p(x)-Laplace thermistor model for electrothermal description of organic semiconductor devices
- Existence of solutions via regularization and Galerkin approximation
- Numerical approximation via hybrid finite-volume/element scheme and numerical path following techniques
- Implemented in software protoype
- Pattern formation in OLEDs can be explained by self-heating, Arrhenius law and sheet resistance

References

Modeling

- Fischer, Pahner, Lüssem, Leo, Scholz, Koprucki, Gärtner, and Glitzky Self-heating, bistability, and thermal switching in organic semiconductors, PRL 110, (2013)
- Fischer, Koprucki, Gärtner, Tietze, Brückner, Lüssem, Leo, Glitzky, and Scholz Feel the heat: Nonlinear electrothermal feedback in Organic LEDs, AFM 24 (2014)
- Liero, Koprucki, Fischer, Scholz, and Glitzky

p-Laplace thermistor modeling of electrothermal feedback in organic semiconductor devices, ZAMP 66, (2015)

Analysis

Glitzky and Liero

Analysis of p(x)-Laplace thermistor models describing the electrothermal behavior of organic semiconductor devices, WIAS-Preprint 2143, (2015)

Bulíček, Glitzky, and Liero

Systems describing electrothermal effects with p(x)-Laplacian like structure for discontinuous variable exponents, WIAS preprint 2206, 2016

Bulíček, Glitzky, and Liero

Thermistor systems of *p*(*x*)-Laplace-type with discontinuous exponents via entropy solutions, WIAS preprint 2247, 2016

New operation mode in spatially dependent setting appears

$$\frac{\mathrm{d}V_i}{\mathrm{d}I_i} = \frac{\mathrm{d}V_i}{\mathrm{d}V_{\mathrm{ext}}} \Big(\frac{\mathrm{d}I_i}{\mathrm{d}V_{\mathrm{ext}}}\Big)$$

| | $rac{\mathrm{d}V_i}{\mathrm{d}V_{\mathrm{ext}}} > 0$ | $rac{\mathrm{d}V_i}{\mathrm{d}V_{\mathrm{ext}}} < 0$ |
|--|---|---|
| $\frac{\mathrm{d}I_i}{\mathrm{d}V_{\mathrm{ext}}}>0$ | I: normal mode | II: S-NDR |
| $\frac{\mathrm{d}I_i}{\mathrm{d}V_{\mathrm{ext}}} < 0$ | not present | III: switched back |

